

# UNENE Graduate Course Reactor Thermal-Hydraulics Design

McMaster University  
Whitby

March 1-2, March 15-16,  
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## Thermal Efficiency

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# Thermal Efficiency – Inlet Pressure

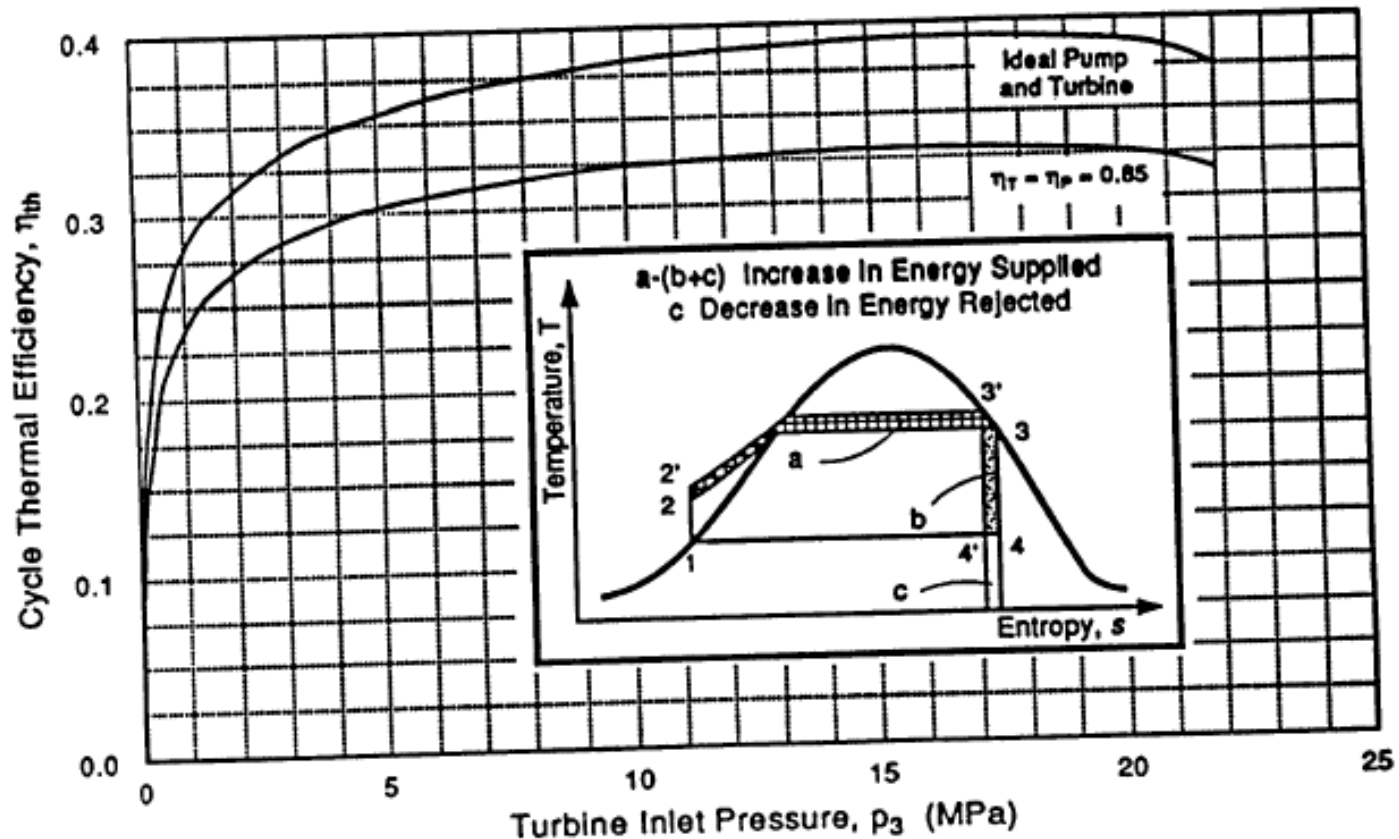


Figure 6-13 Thermal efficiency of Rankine cycle using saturated steam for varying turbine inlet pressure. Turbine inlet: saturated vapor. Exhaust pressure: 7kPa.

# Thermal Efficiency – Outlet Pressure

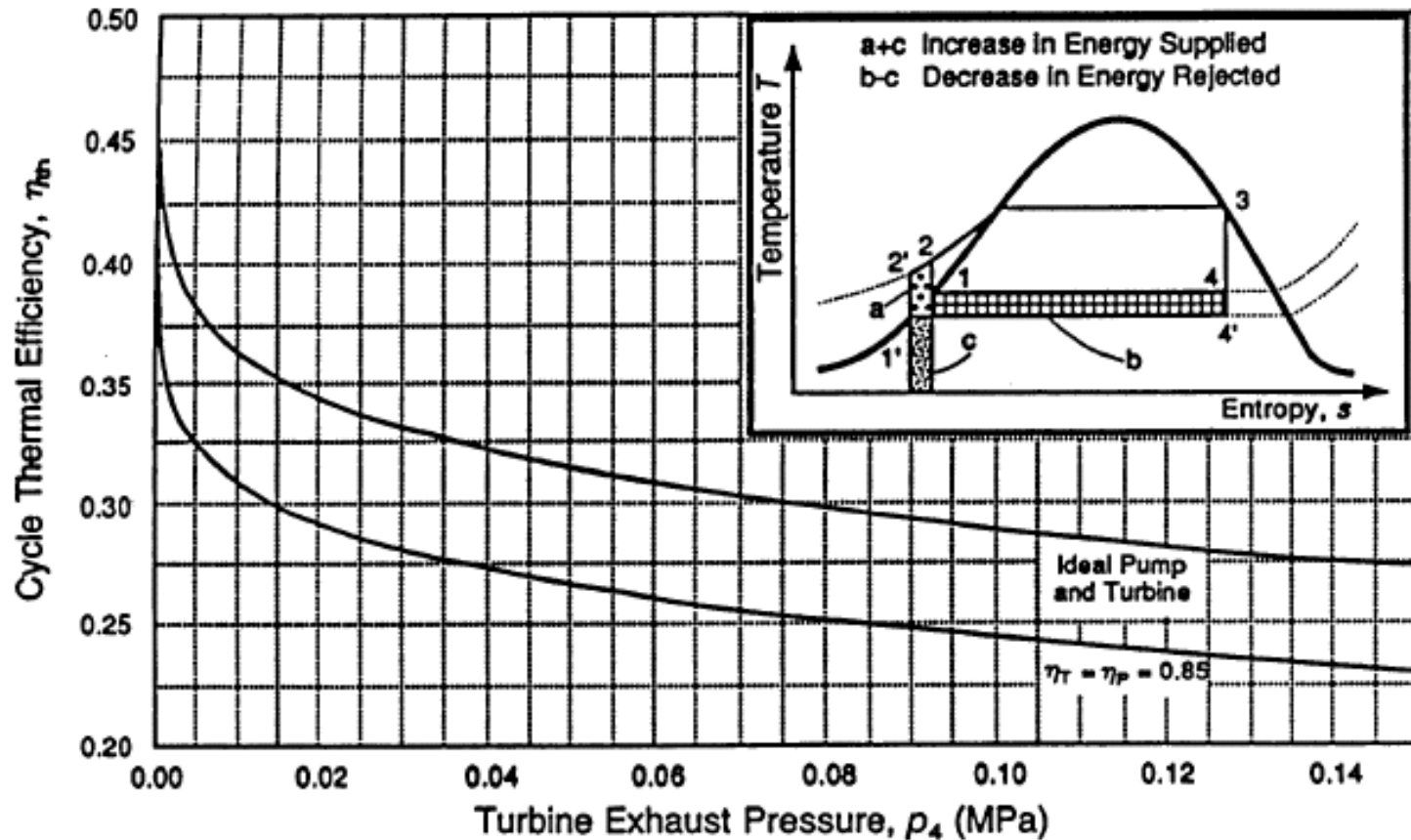


Figure 6-14 Thermal efficiency of Rankine cycle for a saturated turbine inlet state for varying turbine outlet pressure. Turbine inlet: 7.8 MPa saturated vapor.



# Thermal Efficiency – Open Configuration

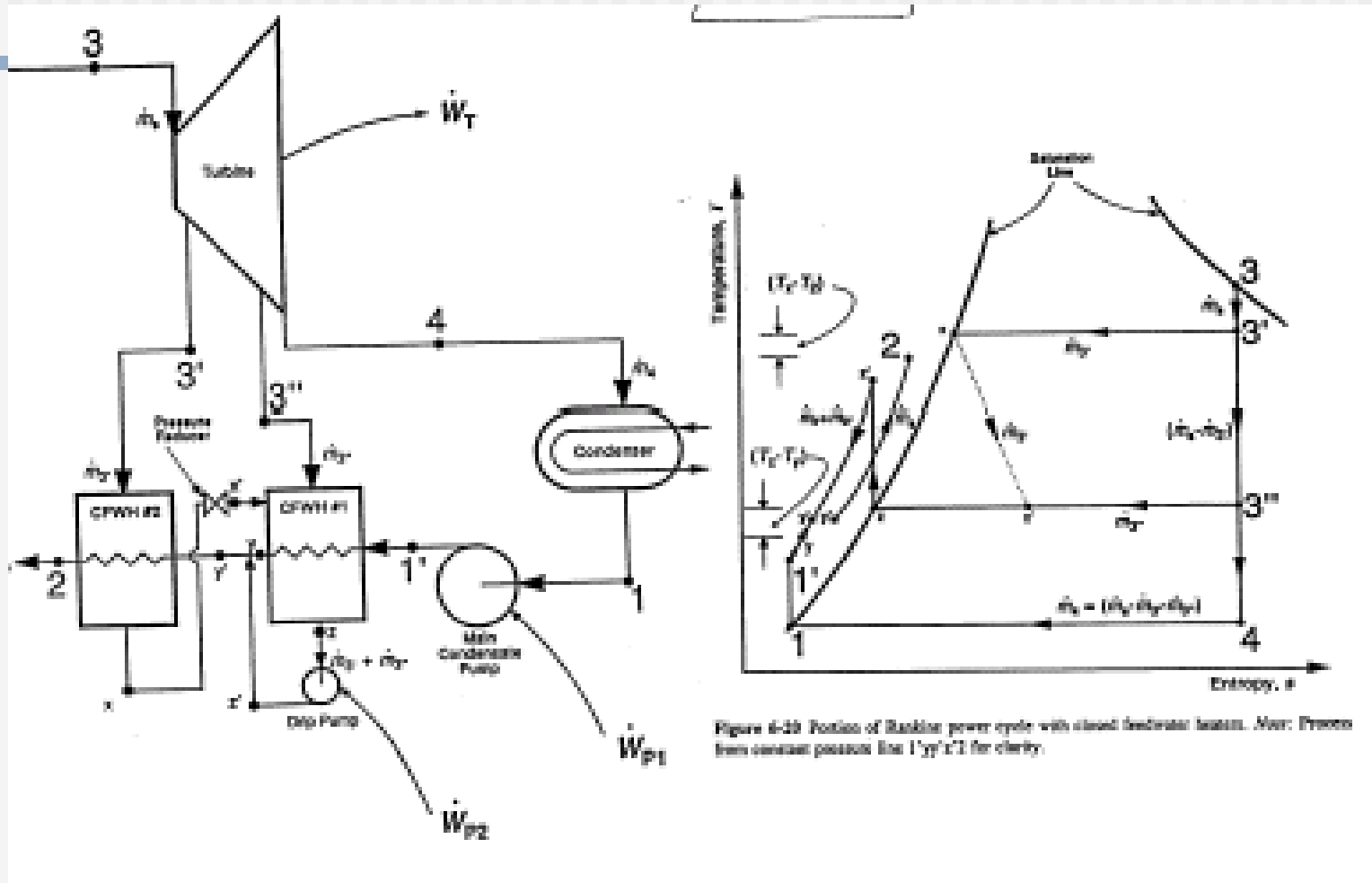
OPEN FEED WATER HEATERS

$$W_T = \dot{m}_3 (h_3 - h_2) + (\dot{m}_5 - \dot{m}_3)(h_3 - h_{3a}) + \dot{m}_4 (h_{3a} - h_4)$$

$$h_2 = \frac{\dot{m}_3 h_{3a} + \dot{m}_4 h_4}{\dot{m}_3 + \dot{m}_4} = \frac{\dot{m}_3 h_{3a} + \dot{m}_4 h_4}{\dot{m}_5 - \dot{m}_3}$$

$$h_3 = \frac{\dot{m}_3 h_{3a} + (\dot{m}_5 - \dot{m}_3) h_{3a}}{\dot{m}_5}$$

# Thermal Efficiency – Closed Configuration



# Thermal Efficiency – Closed Configuration

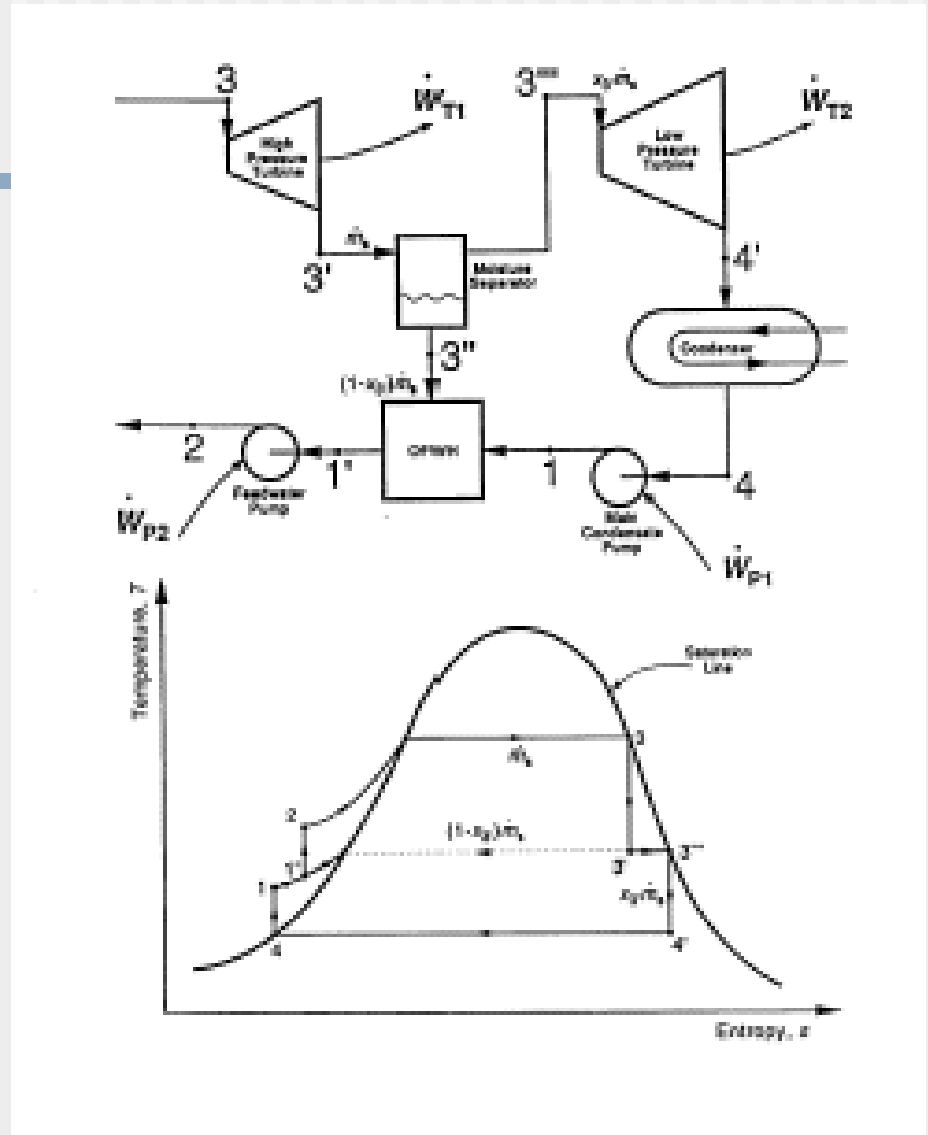
CLOSED FLOW WATER HEATER

$$h_y = \frac{\dot{m}_3 h_{3s} + \dot{m}_4 h_{4s} + \dot{m}_5 h_{5s}}{\dot{m}_4} = (\dot{m}_3 + \dot{m}_5) h_{3s}$$

$$h_{y1} = \frac{\dot{m}_4 h_y + (\dot{m}_3 + \dot{m}_5) h_{3s}}{\dot{m}_2}$$

$$h_2 = \frac{\dot{m}_3 (h_y - h_{3s}) + \dot{m}_2 h_{y1}}{\dot{m}_2}$$

# Thermal Efficiency – Moisture Separation



# Thermal Efficiency – Open Configuration

## MOISTURE SEPARATION

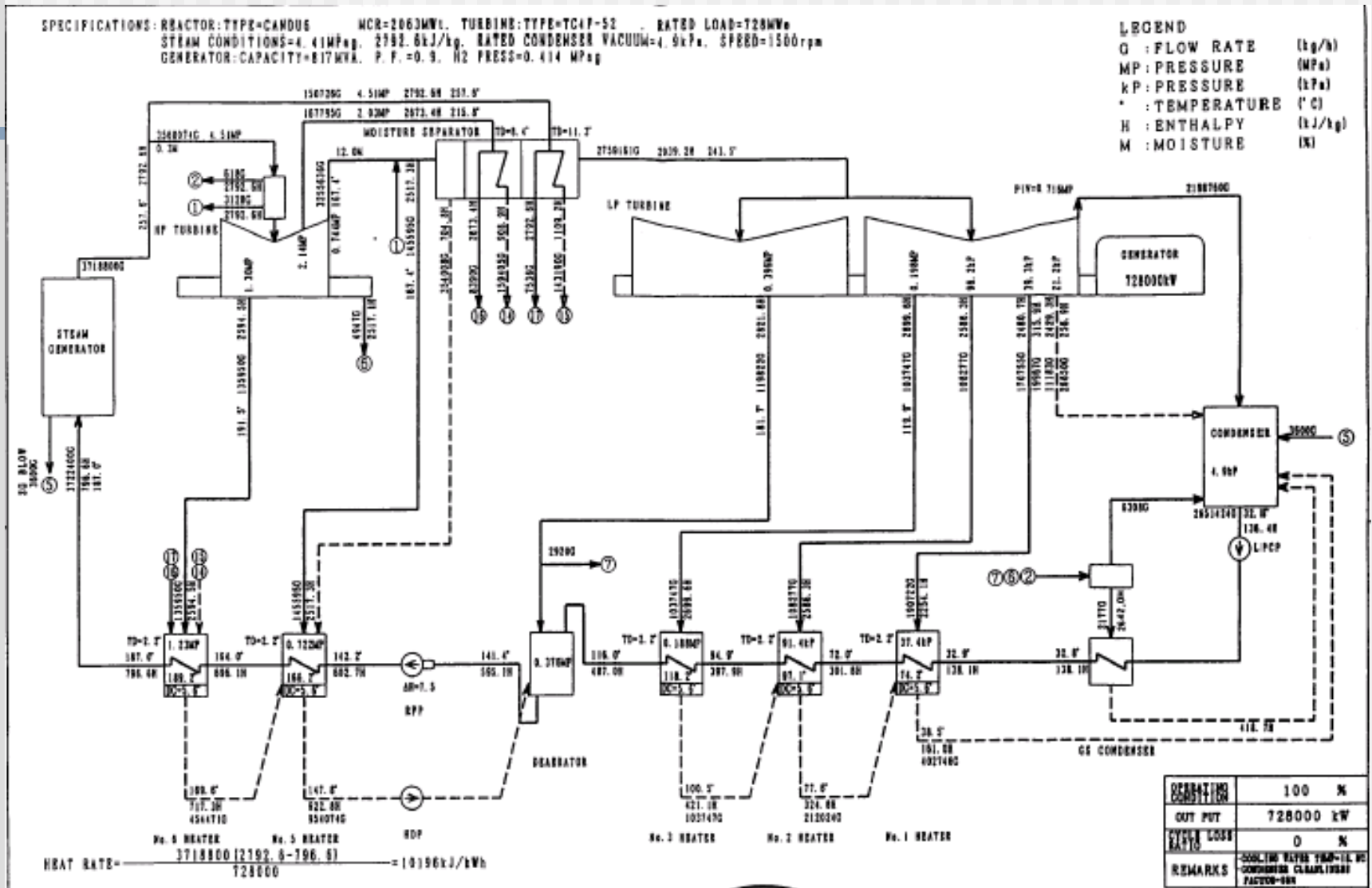
$$h_{3a} = h_f \text{ (at } P_{3a}) \quad (1 - X_{3a}) \dot{m}_5 \text{ saturated}$$

$$h_{3a} = h_g \text{ (at } P_{3a}) \quad X_{3a} \dot{m}_5 \text{ saturated}$$

$$h_{3a} = \frac{h_{3a} (1 - X_{3a}) \dot{m}_5 + h_g X_{3a} \dot{m}_5}{\dot{m}_5}$$



# Thermal Efficiency – CANDU 6



# Questions?

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